

# High Efficiency ZVS-PWM Dual-Output Buck Converters with EMI Reduction Method

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# Outline

- Research Objective
- SISO Converter with ZVS-PWM Control
  - Circuit and Operation
  - Simulation and Experimental Results
- Proposed SIDO Converter with ZVS-PWM Control
  - Circuit and Operation
  - Simulation Results
- New EMI Reduction Method
  - Spread Spectrum in Switching Converter
  - Simulation Results
- Conclusion

ZVS : Zero Voltage Switching
SISO: Single Inductor Single Output
SIDO: Single Inductor Dual Output
EMI : Electro-Magnetic Interference

# Background

Many DC-DC Converters in Cell phones, manufacturing machinery, etc.

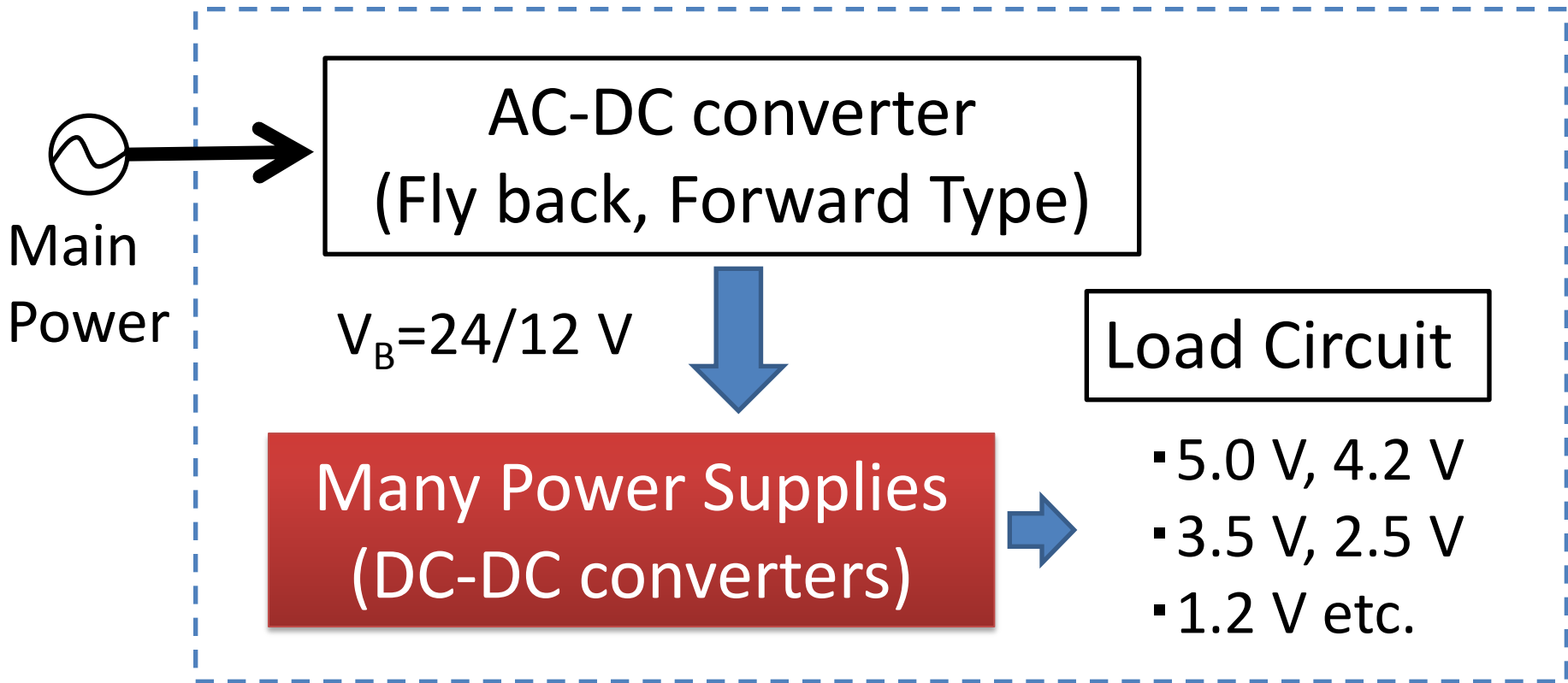


Fig.1 background

- 1) Low Cost, Size, Weight, etc.
- 2) Function: Ripple, Efficiency, EMI

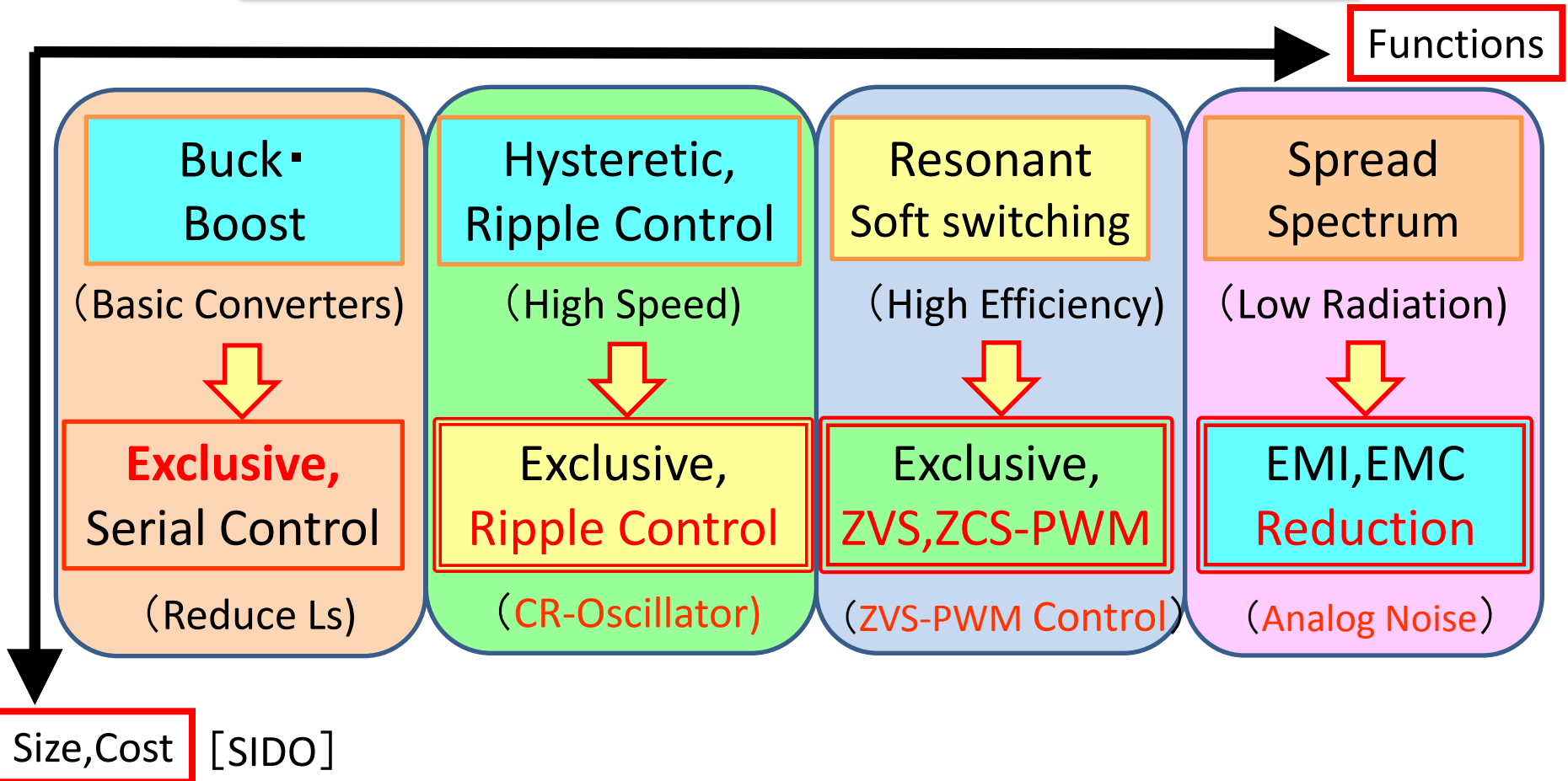


Fig. 2 Research Direction of Switching Converters

\* ZVS: Zero-Voltage Switching  
\* ZCS: Zero-Current Switching

\* SISO: Single Inductor **Single** Output  
\* SIDO: Single Inductor **Dual** Output

\* EMI: Electro-Magnetic Interference  
\* EMC: Electro-Magnetic Compatible

# Research Objective

- SIDO Converter with ZVS-PWM Control

  - Experimental SISO converter with **ZVS-PWM**

  - Our Previous SIDO converter with **Exclusive Control**



- ★ New SIDO Converter with **ZVS-PWM Control**

  - Using no clock

- ★ New **EMI Reduction** with Pseudo Analog Noise

  - Adding analog noise to the reference voltage

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# SISO Buck Converter with ZVS-PWM Control

## 1. Circuit and Operation

### 1) Normal Buck Converter (No Resonant)

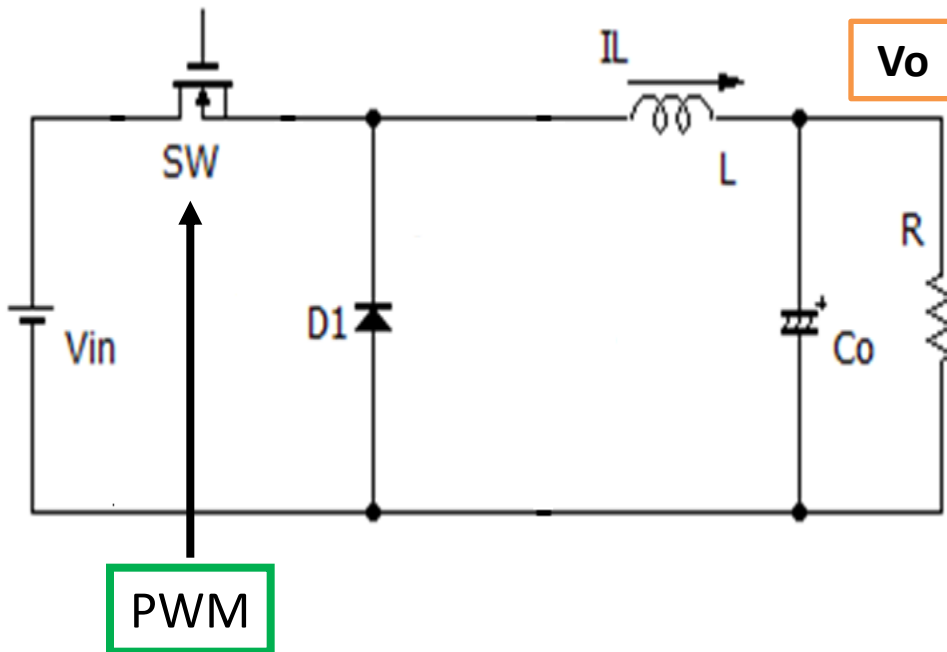


Fig.3 Circuit of Normal Buck Converter

Duty Ratio:  $H \Rightarrow V_o \uparrow$   
 $H \Rightarrow V_o \downarrow$

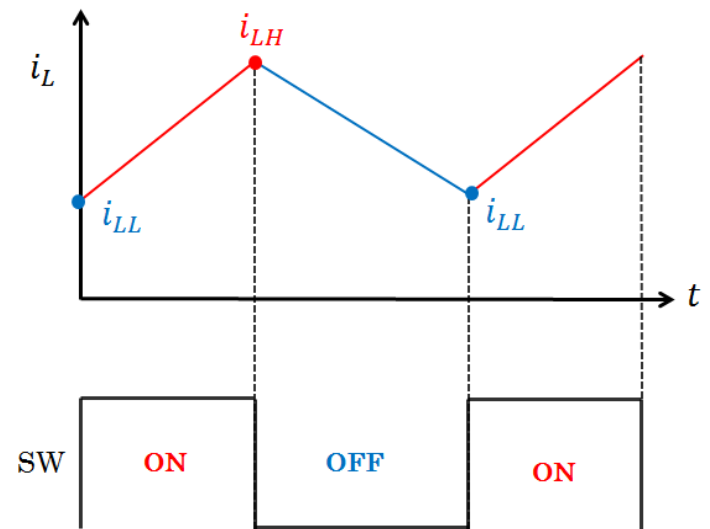


Fig.4 Timing Chart

# SISO Buck Converter with ZVS-PWM Control

## 2) Circuit of Buck Converter with ZVS-PWM

- Circuit: Adding Resonant Capacitor & Body Diode

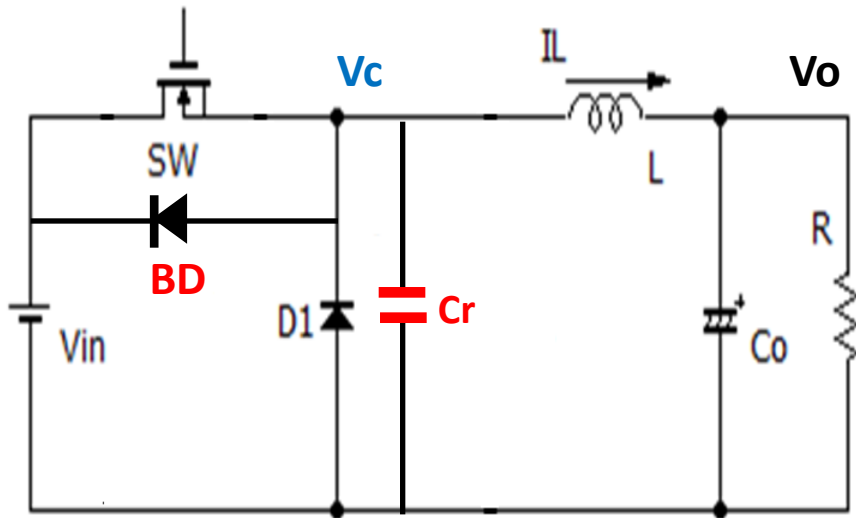


Fig.5 Circuit of Normal Buck Converter

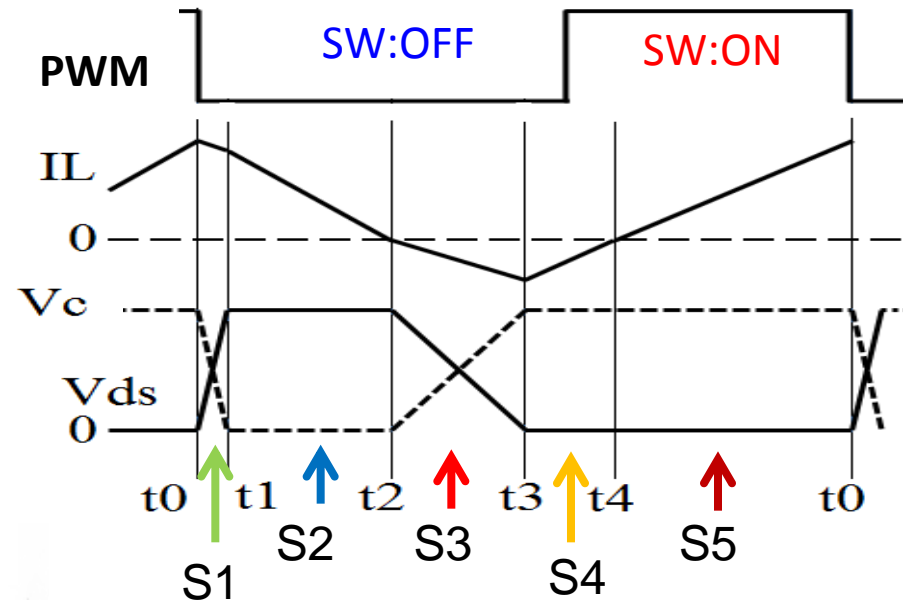


Fig.6 Waveform of Major Signals



### 3) Operation of ZVS-PWM Converter

★ **State 1:** PWM turns to OFF

Current flows from  $C_r$  to  $C_o$  and  $V_c$  decreases.

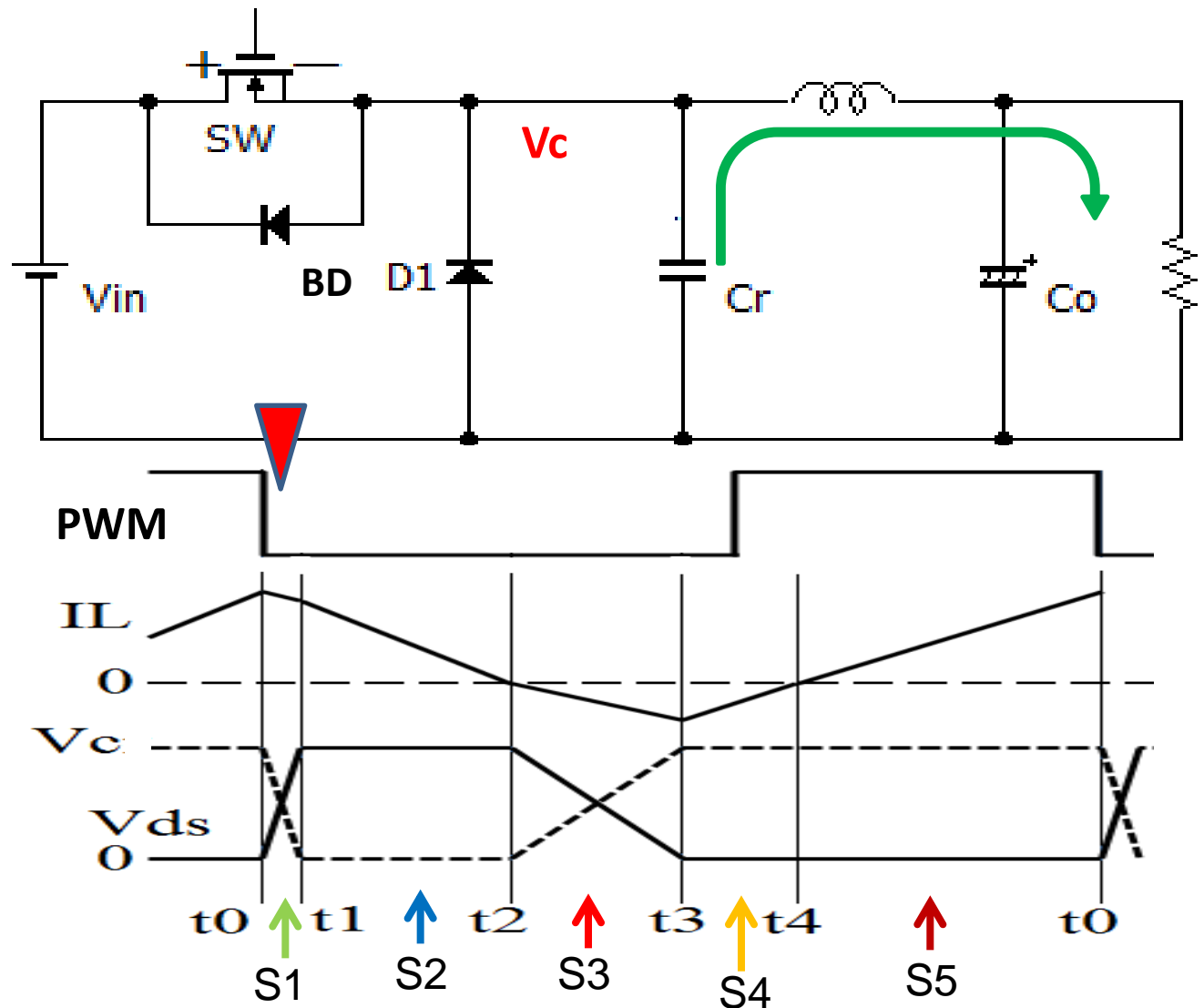


Fig.6 Major Signals

### 3) Operation of ZVS-PWM Converter

★ **State 2:** PWM keeps OFF and  $V_c$  has reached 0V.

D1 turns ON and Inductor is discharging energy via D1.

$V_o$  is increasing.

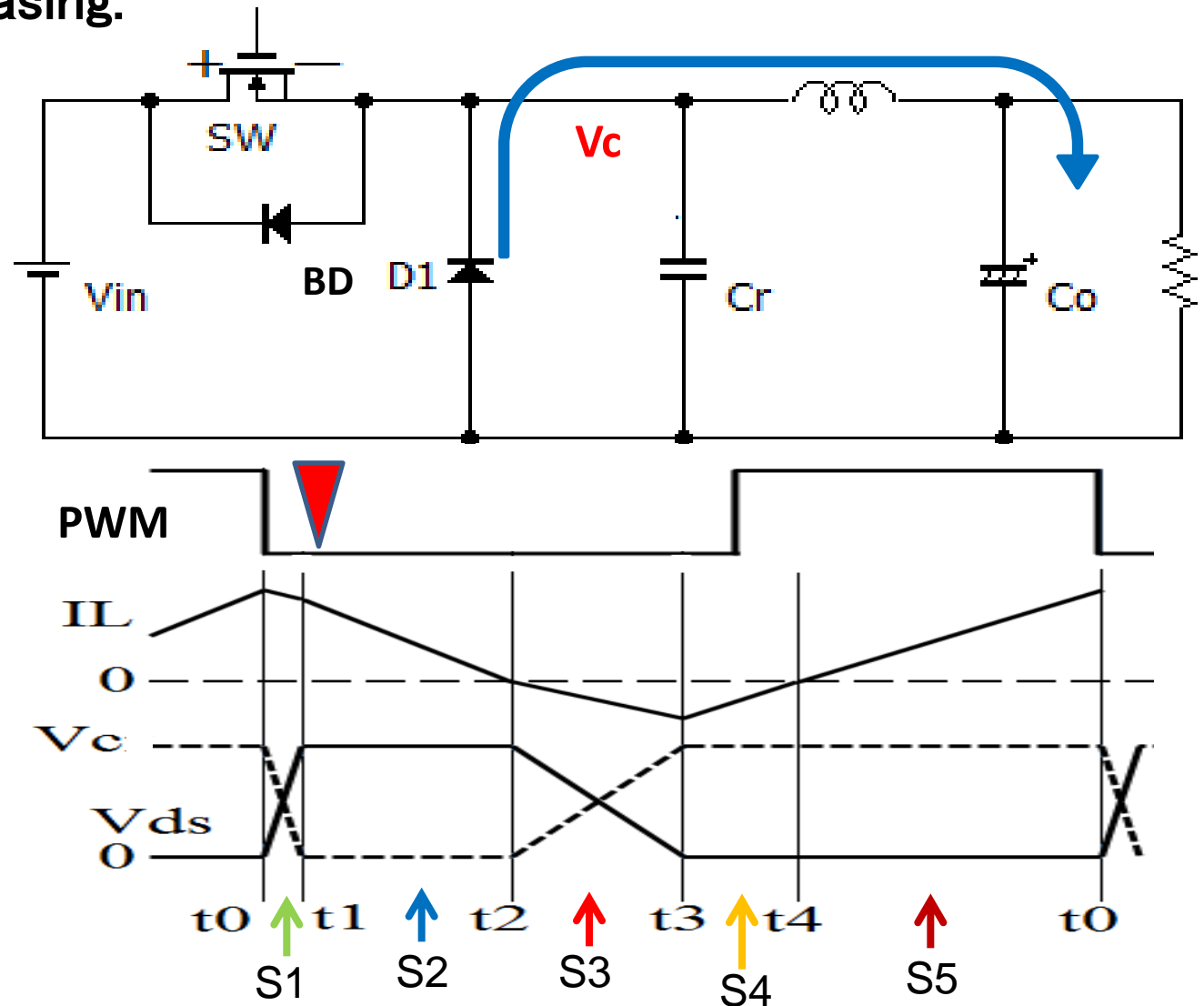


Fig.6 Major Signals

### 3) Operation of ZVS-PWM Converter

- ★ **State 3:** PWM keeps OFF and Inductor has discharged all energy.  $I_L$  flows reverse direction and  $C_r$  is charging.  $V_c$  is increasing.

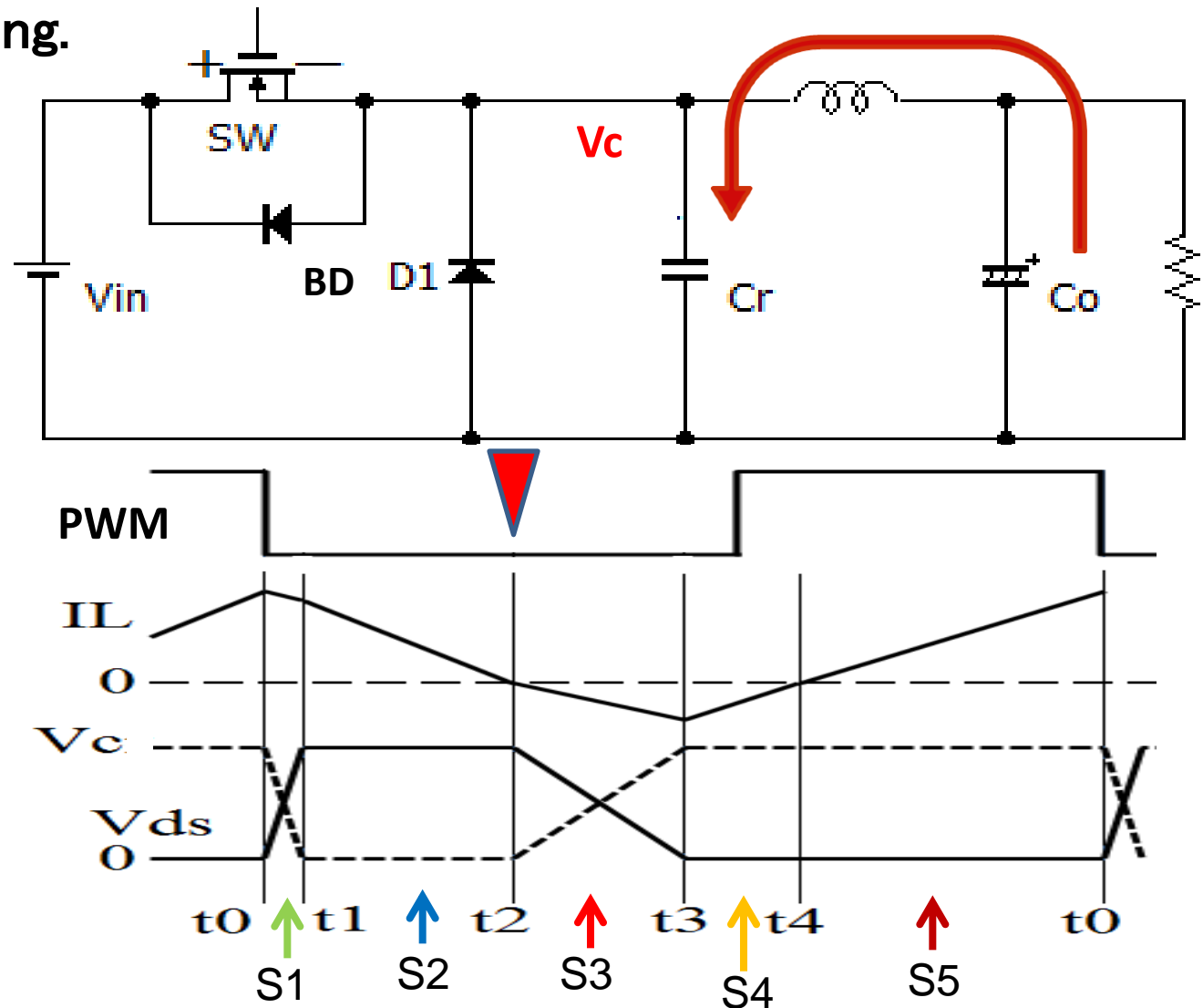


Fig.6 Major Signals

### 3) Operation of ZVS-PWM Converter

★ **State 4:**  $V_c$  has reached to  $V_{in}$  and BD turns ON.

Negative flow of  $I_L$  is decreasing to 0A. PWM turns Hi and SW turns ON.

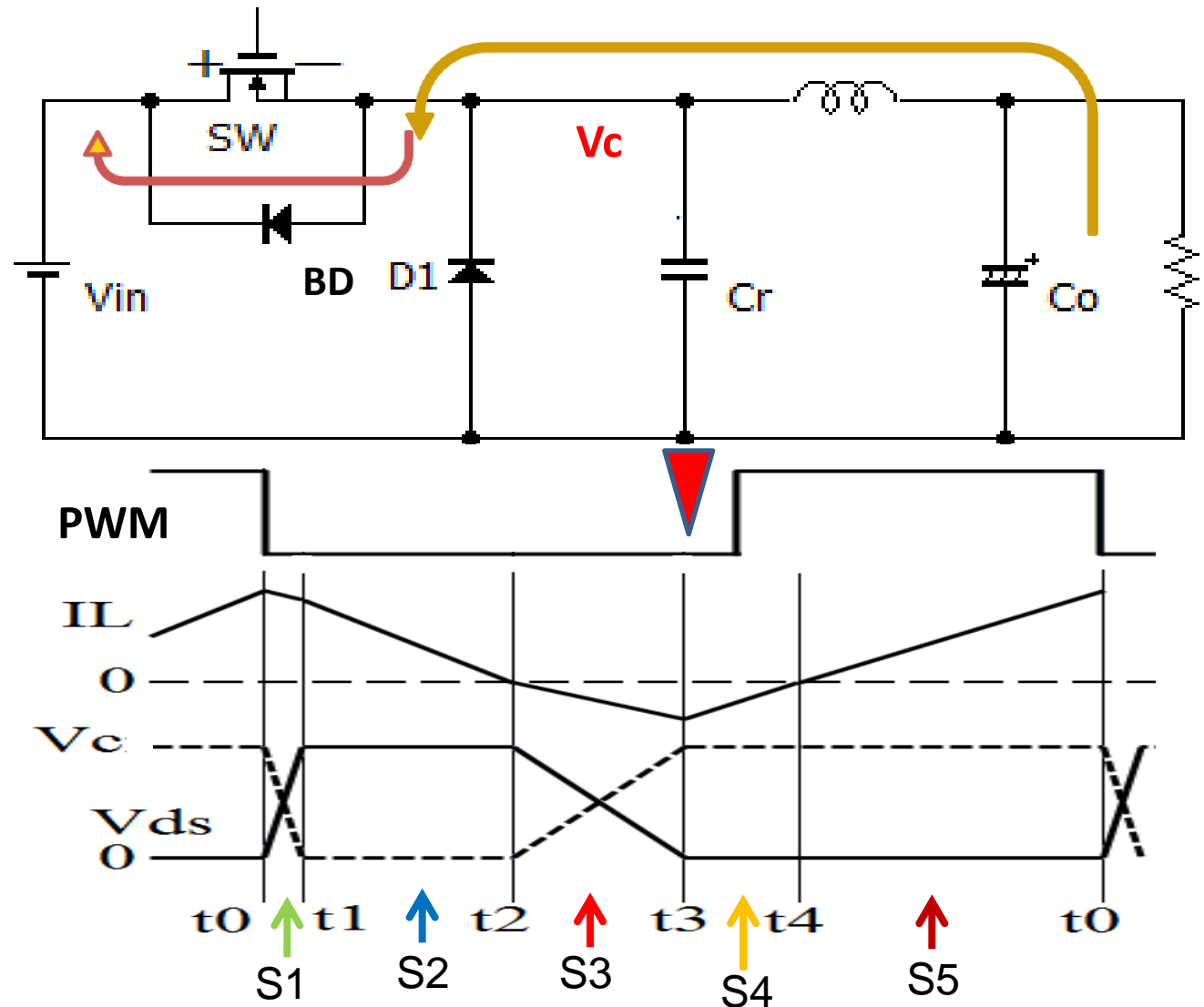


Fig.6 Major Signals

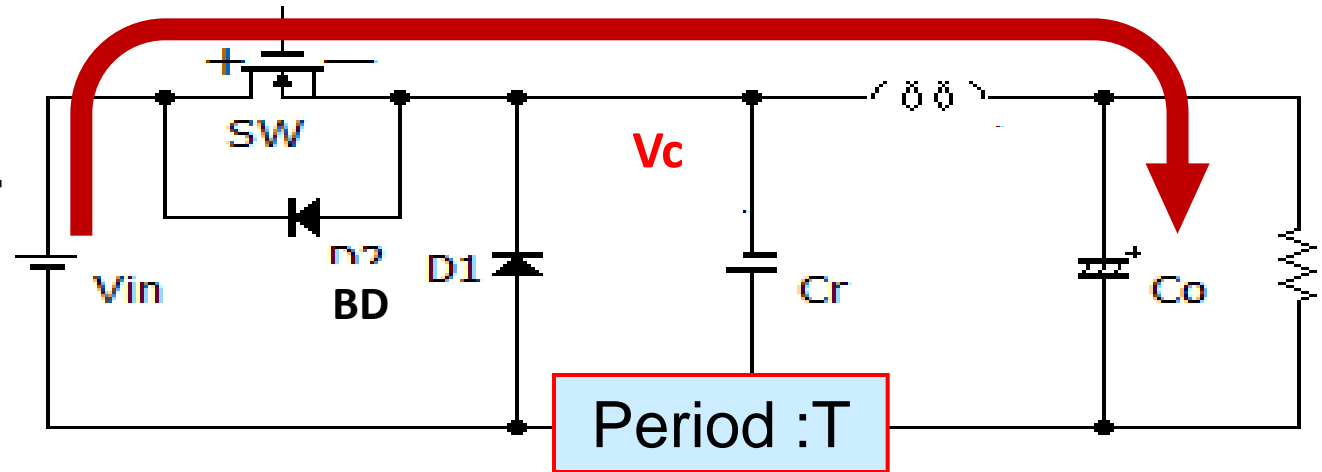
### 3) Operation of ZVS-PWM Converter

★ **State 5:** PWM keeps Hi and SW keeps ON.

$I_L$  is increasing until  $V_o$  reaches reference voltage.

PWM turns Lo.

Then return to S1.



Period depends on  $C_r$ ,  $L$ ,  $V_{in}$ ,  $V_o$ ,  $I_o$ .

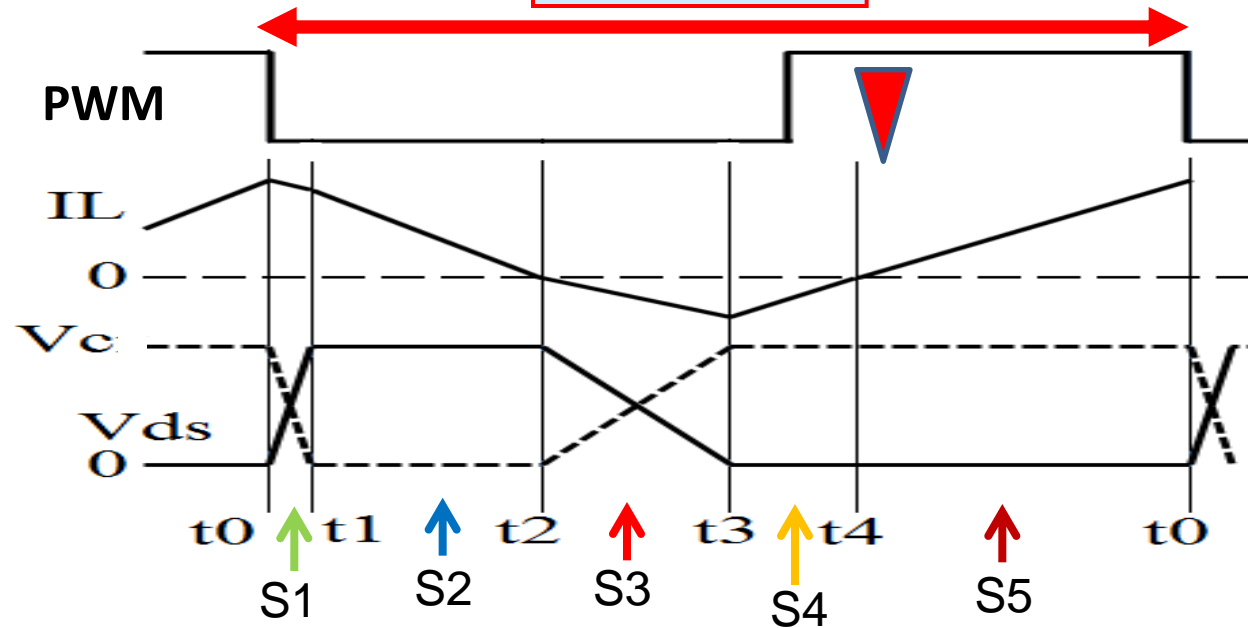


Fig.6 Major Signals

# SISO Buck Converter with ZVS-PWM Control

## 2. Simulation Results

- $V_o$  is compared with  $V_{ref}$  and amplified.
- Then compared with Saw-tooth signal and get PWM pulse.

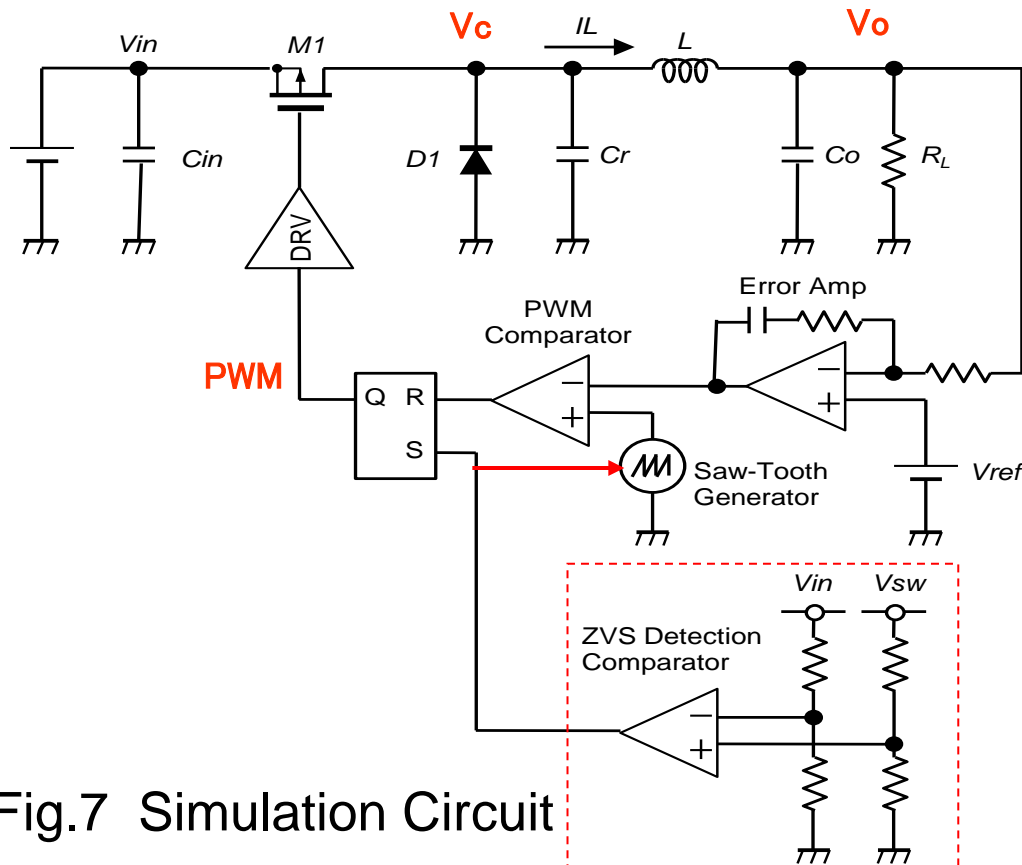


Table 1. Simulation Parameters

Parameter	Value
$V_{in}$	10 V
$V_o$	6.0 V
$L$	1.0 $\mu$ H
$C_r$	47 nF
$C_o$	470 $\mu$ F
$I_o$	0.30 A

Fig.7 Simulation Circuit

# SISO Buck Converter with ZVS-PWM Control

## 2. Simulation Results

- \*  $V_o$  is stable at 6.0V.
- \*  $I_L$  flows positive and negative.
- \* PWM width is determined by feedback loop.

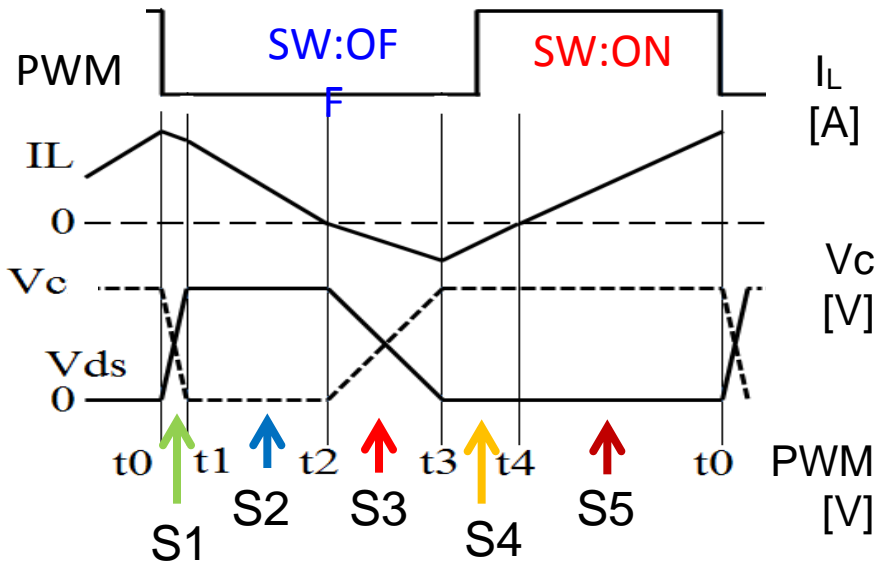


Fig.6 Major Signals

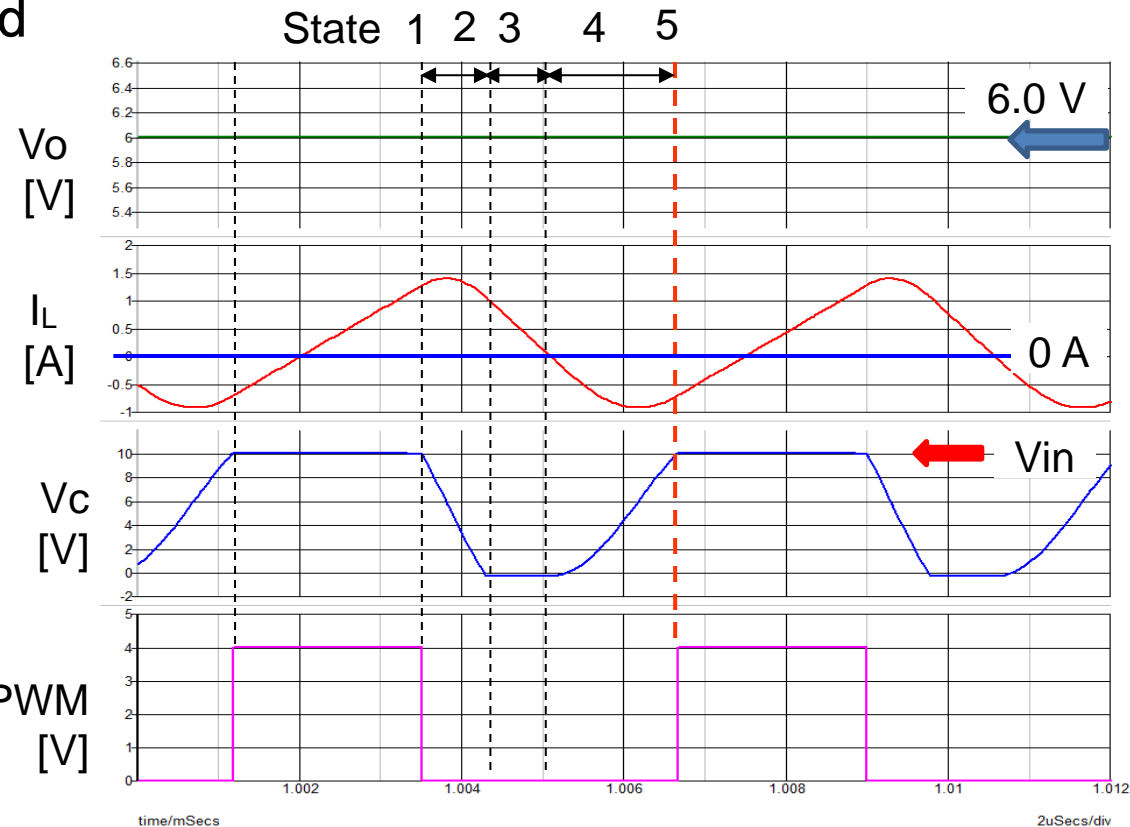


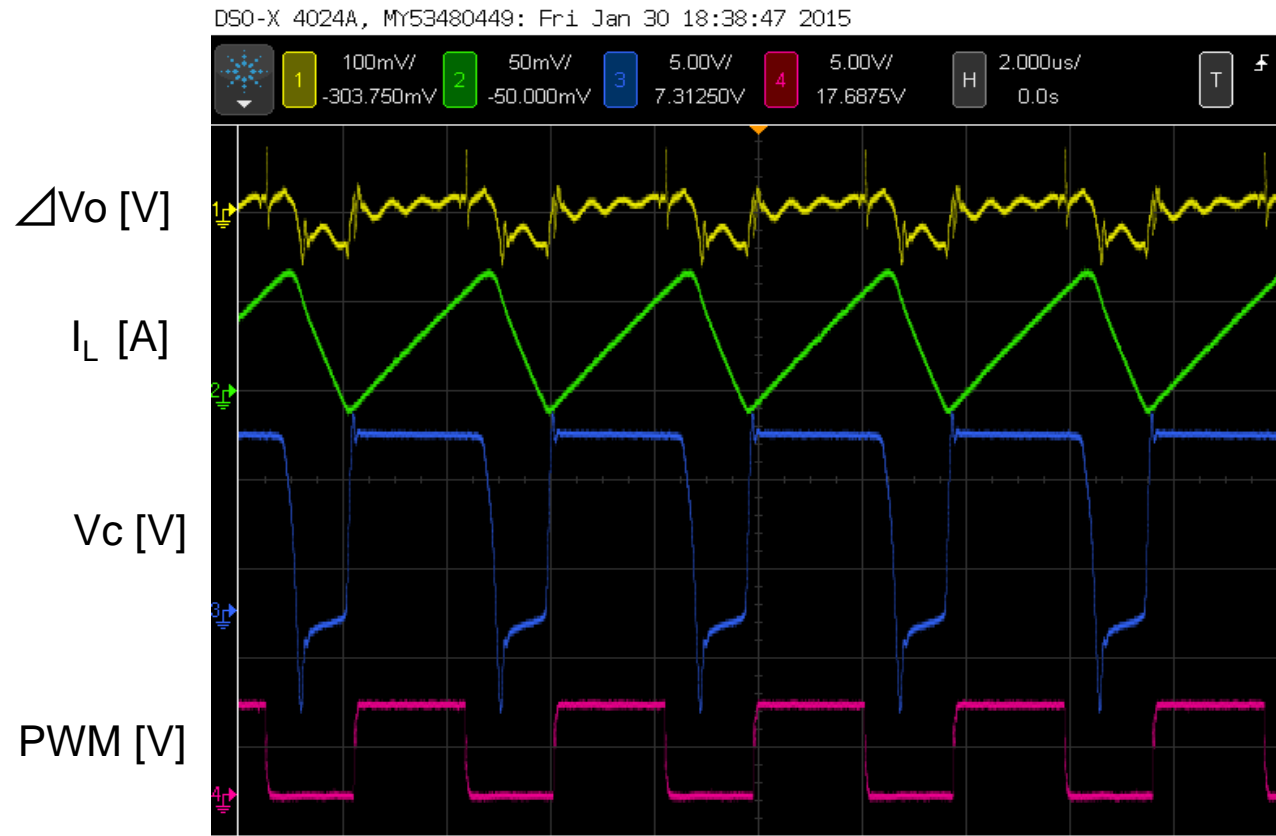
Fig.8 Simulation Result (Major signals) 15

# SISO Buck Converter with ZVS-PWM Control

## 3. Experimental Results

- \* Output ripple: 50mV
- \*  $I_L$  peak : 7.0 A
- \* Fop: 250 kHz

$V_i=10$  V,  $V_o=6.0$  V,  $I_o=0.3$  A



- ▼ Most of ripple is because of ground line impedance.  
This circuit is made on universal board.

Fig.9 Experimental Results



# SISO Buck Converter with ZVS-PWM Control

\* Voltage & Current

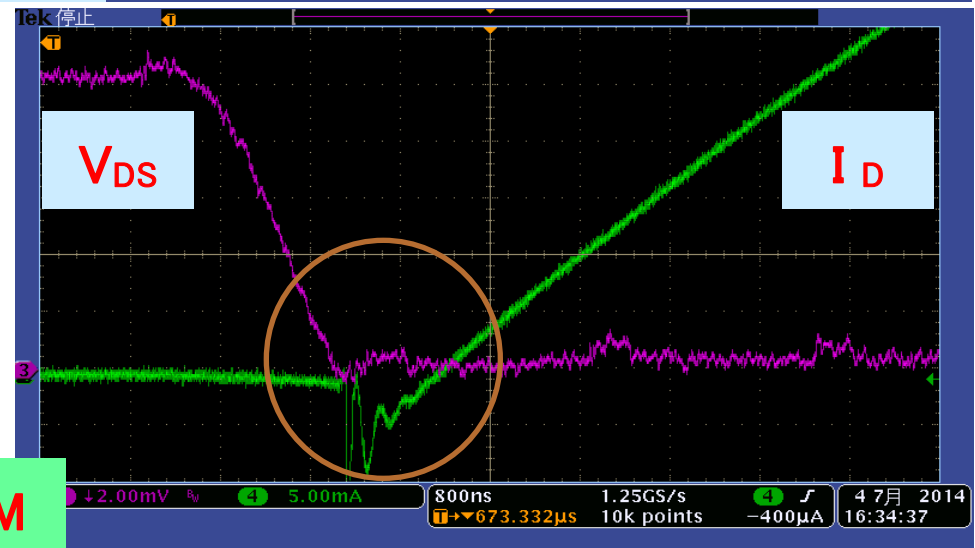
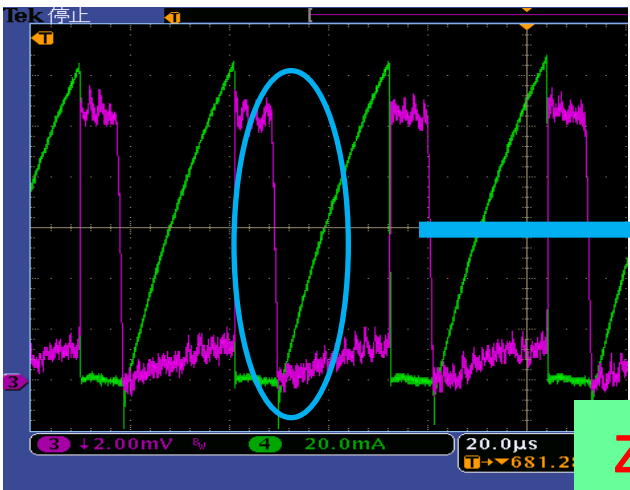
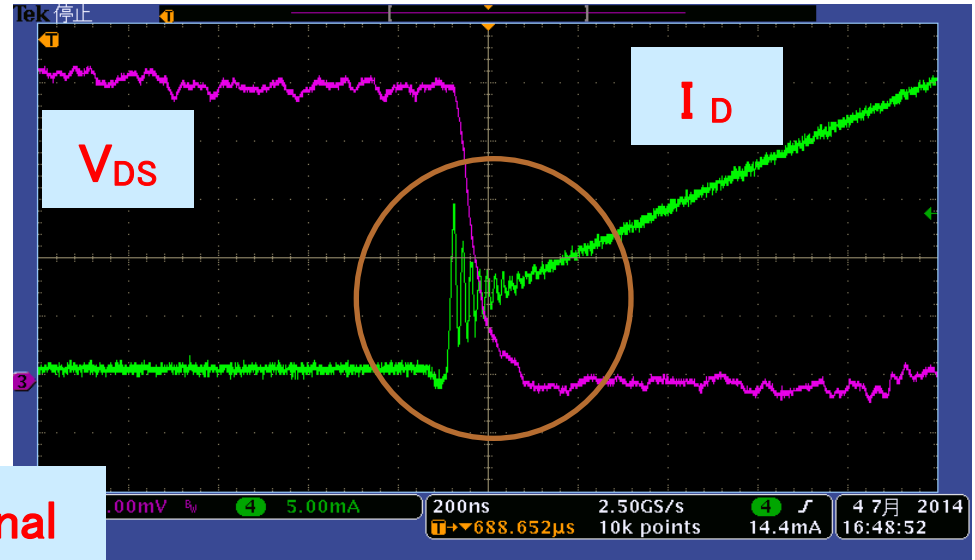


Fig.10 Waveform of Switching Voltage & Current

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  - Simulation Results
- **New EMI Reduction Method**
  - Spread Spectrum in Switching Converter
  - Simulation Results
- Conclusion

# Proposed **SIDO** Converter with ZVS-PWM Control

## 1. Circuit and Operation (1)

- \* Two sub-converters are selected by SEL signal.
- \* SEL signal is made by comparing  $\Delta V1$  &  $\Delta V2$ .  
Sub-conv. 1 is selected when  $\Delta V1 > \Delta V2$ .
- \*  $V1 > V2$ .

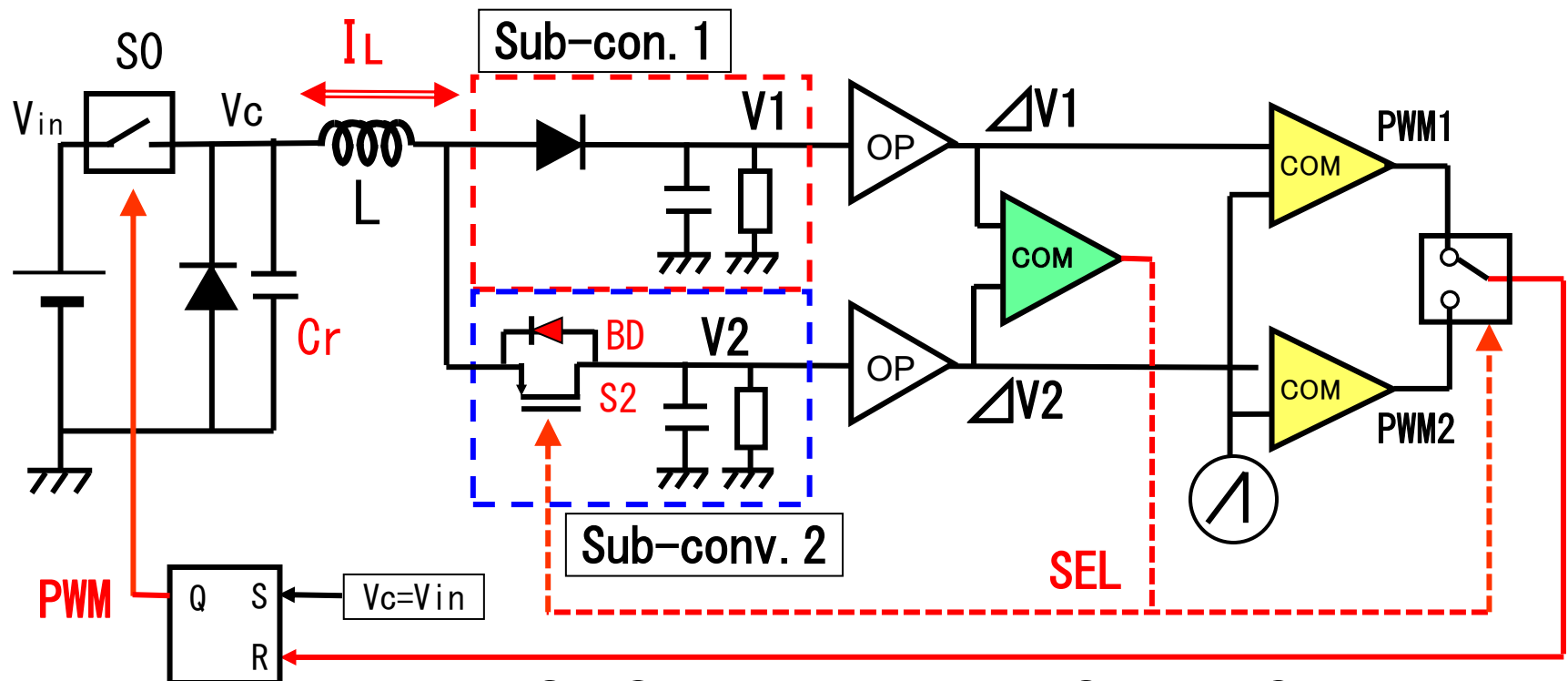


Fig.11 SIDO Converter with ZVS-PWM Control

# Proposed **SIDO** Converter with ZVS-PWM Control

## 1. Circuit and Operation (2)

\* Sub-converters are selected with SW2 and Di.

\* Inductor Current **IL** flows forward & reverse.

**Body Di** is important for **reverse IL** when con.1 is selected.

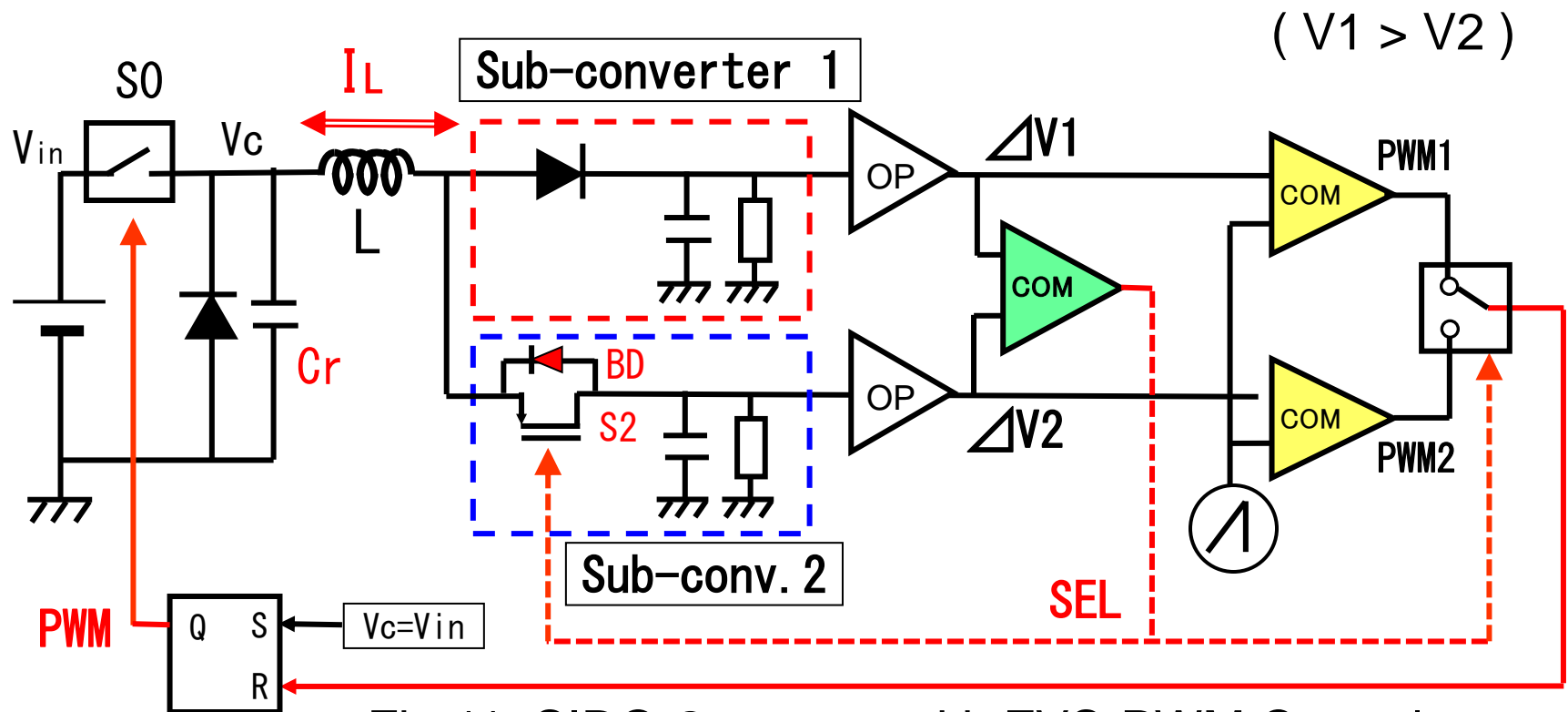


Fig.11 SIDO Converter with ZVS-PWM Control

# Proposed **SIDO** Converter with ZVS-PWM Control

## 2. Simulation Results (1)

- $V_i=10V$   
     $\Rightarrow V_1=6.0V, V_2=5.5V$
- $I_{o1}=I_{o2}=0.5A$
- $L=2.2\mu H,$   
     $C_r=1.0nF, C=470\mu F$

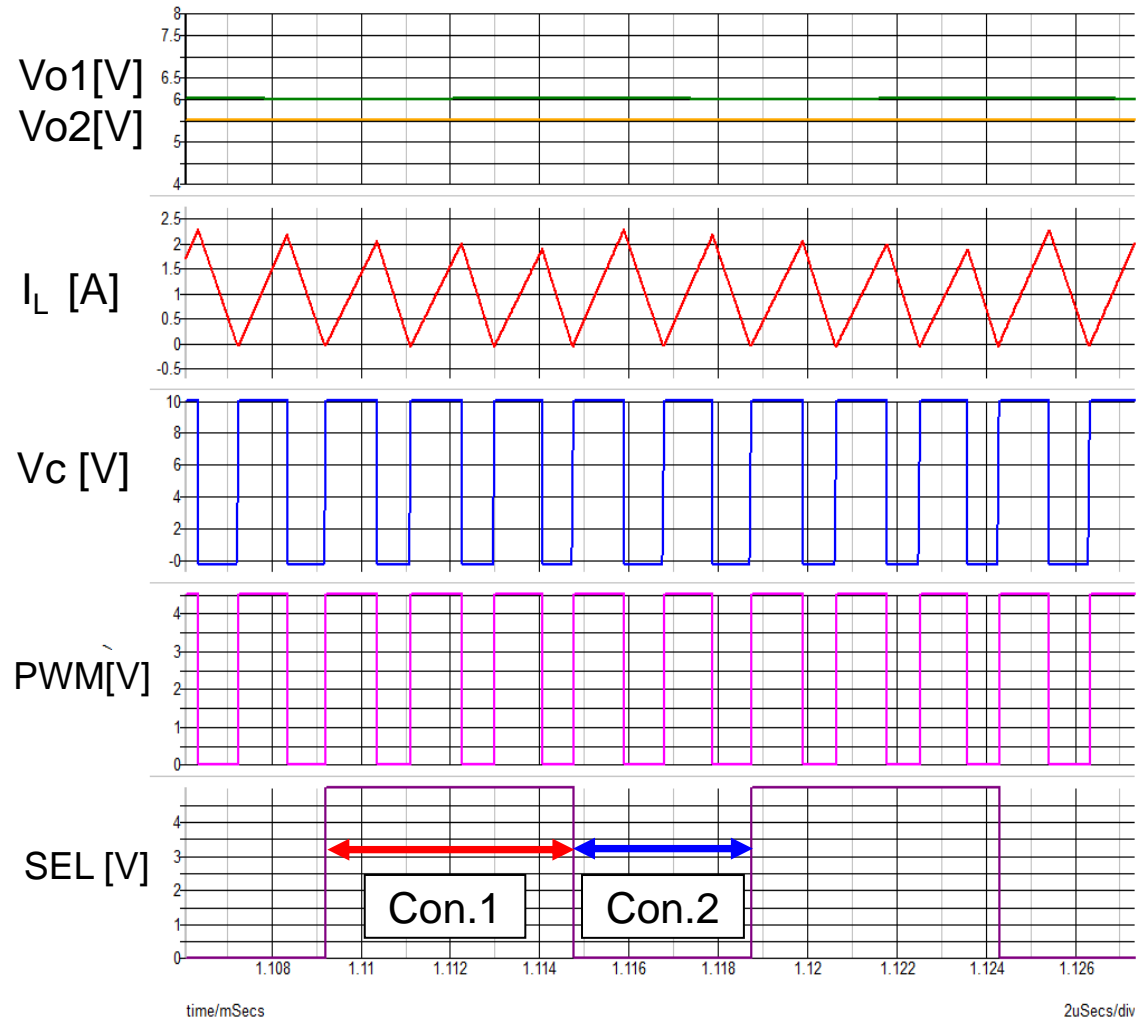


Fig.12 Simulation Result

# Proposed **SIDO** Converter with ZVS-PWM Control

## 2. Simulation Results (2)

- Output Voltage Ripple  
 $\Delta V_1, \Delta V_2 < 10\text{mV}$
- Over-shoot  $\doteq \pm 10\text{ mV}$

\* Self-reg. > Cross-reg.

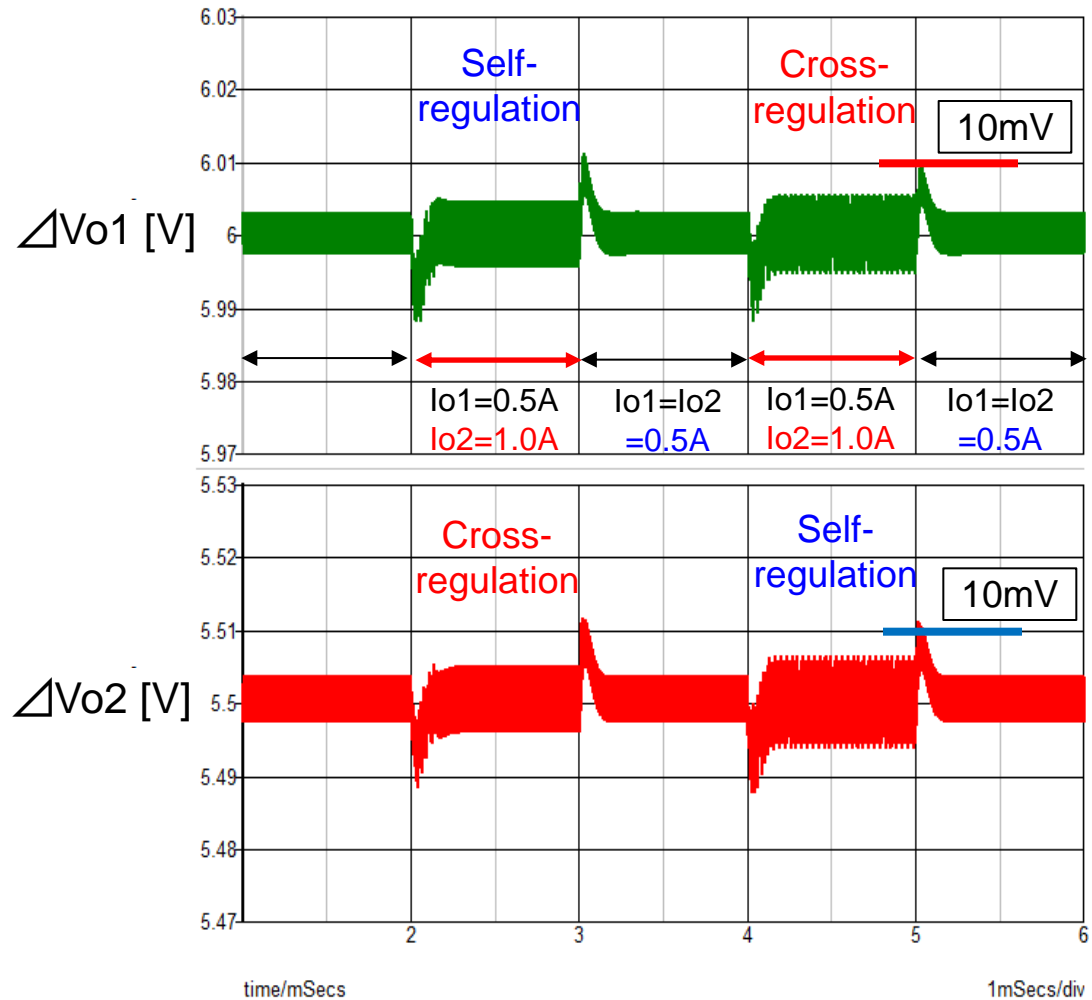


Fig.13 Simulation Results (Ripples)

# Proposed **SIDO** Converter with ZVS-PWM Control

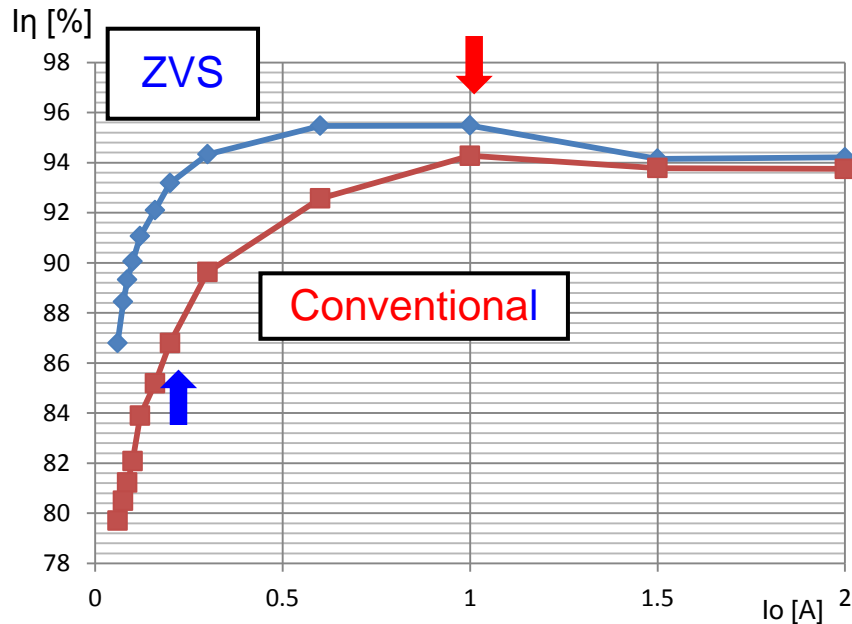
## ● Efficiency vs. $I_o$ of Converters

\* **SISO** Converter : MAX 95.5% (Conventional : MAX 94.3%) @  $I_o=1.0A$

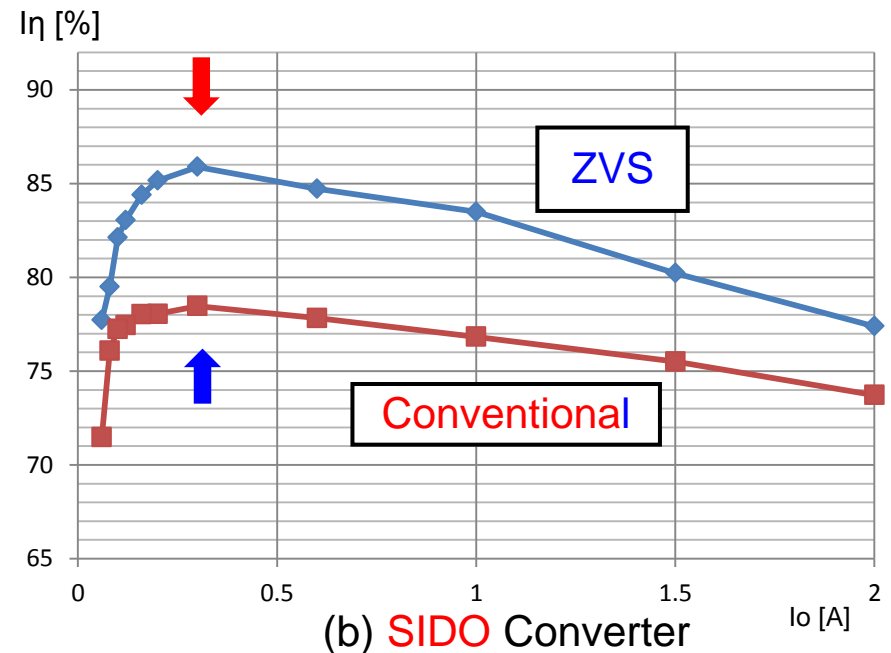
$\Delta \eta = 1.2\%$  @  $I_o=1.0A$ , MAX  $\Delta \eta = 6.5\%$  @  $I_o=0.2 A$

\* **SIDO** Converter : MAX 86.0% (Conventional : MAX 78.5%) @  $I_o=0.3A$

$\Delta \eta = 7.5\%$  @  $I_o=0.3 A$



(a) **SISO** Converter



(b) **SIDO** Converter

Fig.14 Efficiency of ZVS-PWM Converter

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- **New EMI Reduction Method**
  - Spread Spectrum in Switching Converter
  - Simulation Results
- **Conclusion**



# New EMI Reduction Method

## 1. Spread Spectrum in Switching Converters

● Method: **Random Shift of PWM Phase**

\* Conventional Method: **Digital Spread Spectrum**

▪ Many Shift-registers & Selectors:  $10 \sim 12$ bits

\* Our Previous Method: **Analog Noise Spread Spectrum**

▪ Only **3-bit Counter + LPF Circuit**  $\Rightarrow$  Shift PWM

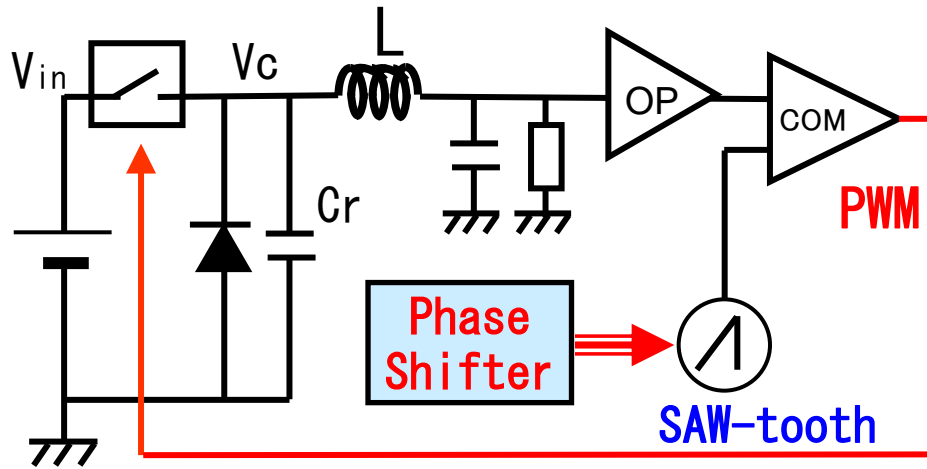


Fig.16 Converter with Spread Spectrum

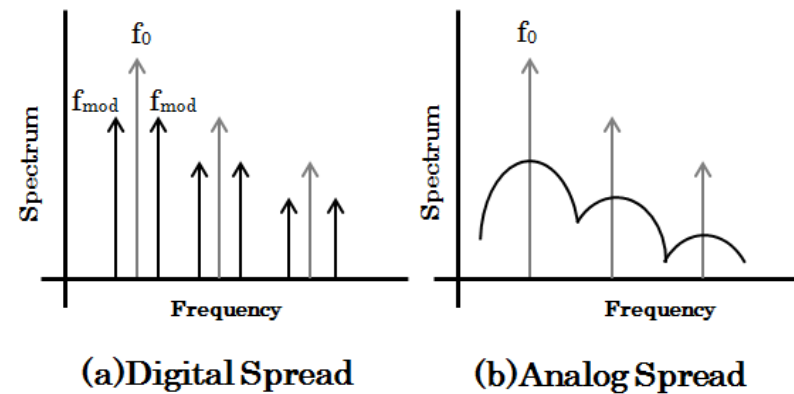


Fig.17 Spread Spectrum

# New EMI Reduction Method

## 2. M-sequence Circuit : Digital Random Noise Generator

### ● Circuit & Operation

\* Shift-registers & Ex-OR gate:

\*  $N=(2^n - 1)$  levels on bit number n of primitive polynomial

$$G(x) = x^3 + x^2 + 1 \quad (3\text{-bit} \Rightarrow 7 \text{ level})$$

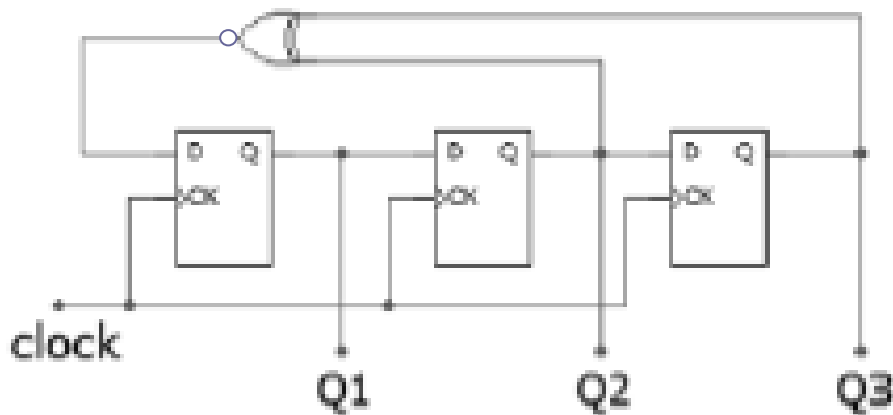


Fig.18 M-sequence Circuit

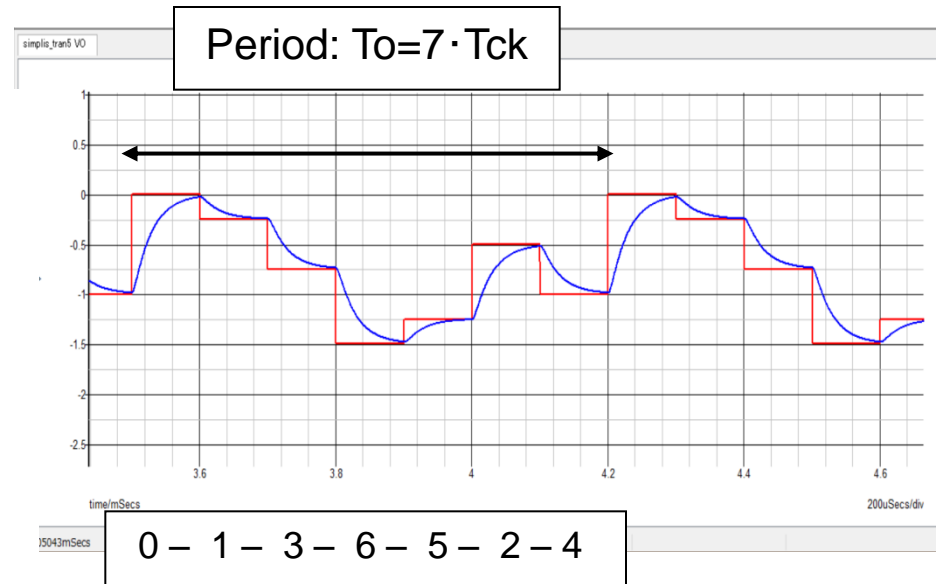


Fig.19 Output Step Pattern

# New EMI Reduction Method

## 3. Proposed Spread Spectrum with New Noise Generator

\* ZVS-PWM Converter is difficult to shift the PWM phase because of **no clock, no synchronized signal**.

\* Add analog noise to **Voltage Reference**

SAW is not constant phase  $\longleftrightarrow$  Error voltage is dithered

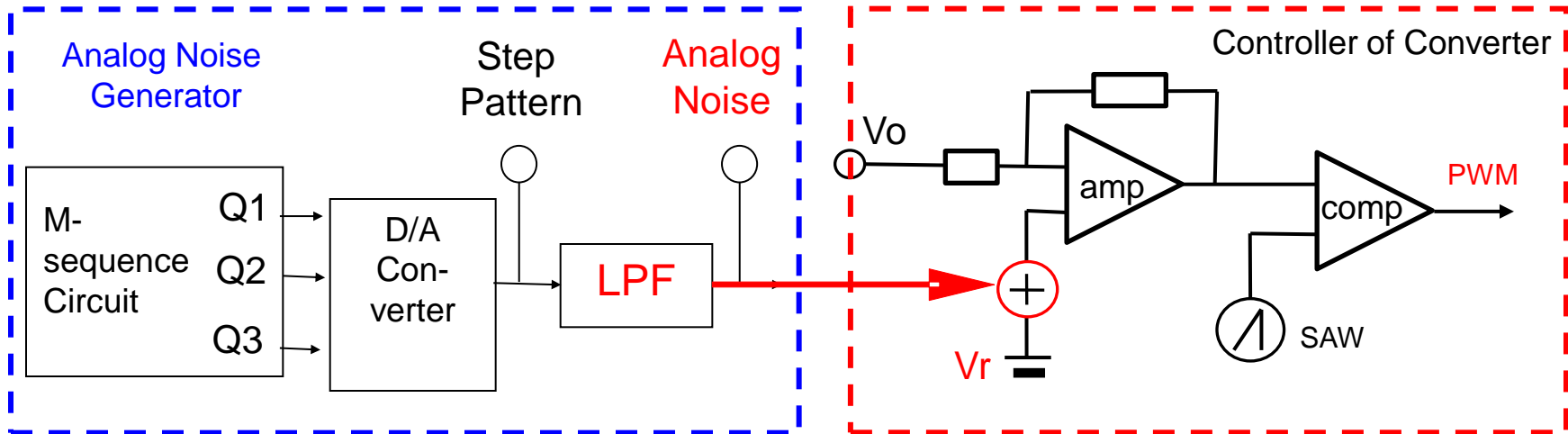


Fig.20 Spread Spectrum by Adding Analog Noise

# New EMI Reduction Method

## 3. Simulation Results

- Output Voltage Ripple
  - $\Delta V_o = 10\text{mV}_{pp}$  ( $< 0.2\%$  of  $V_o$ )
- Effect of Spread Spectrum
  - \* Peak level :  $-4.0\text{dB}$ 
    - $1.2\text{V} \leftarrow 3.0\text{V}$  ( $F = 377\text{ kHz}$ )
  - \* Harmonic level :  $-3.5\text{dB}$ 
    - $0.4\text{V} \leftarrow 0.9\text{V}$  ( $F = 1.13\text{MHz}$ )

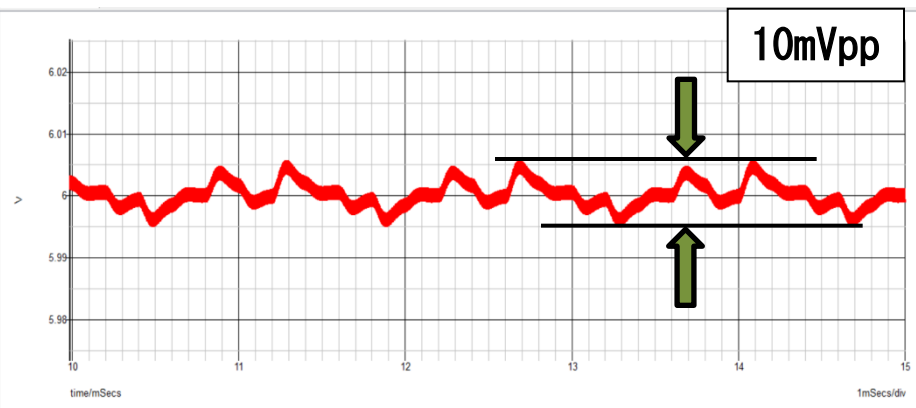
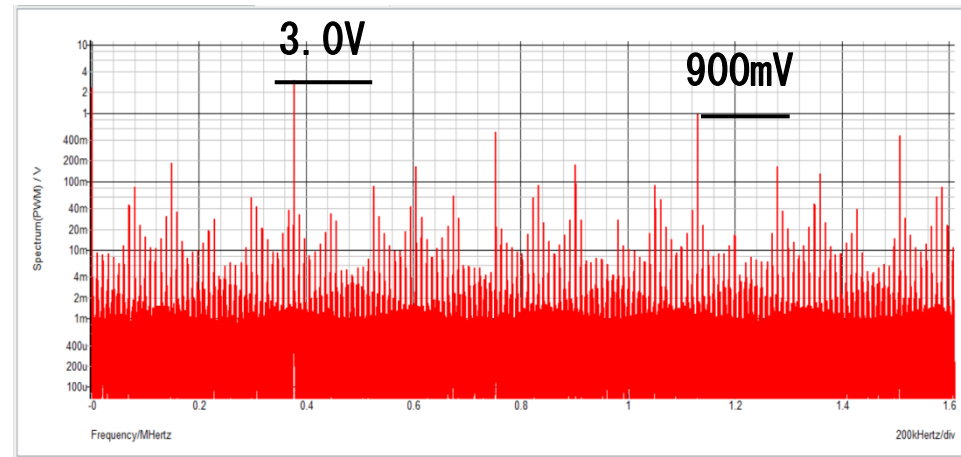
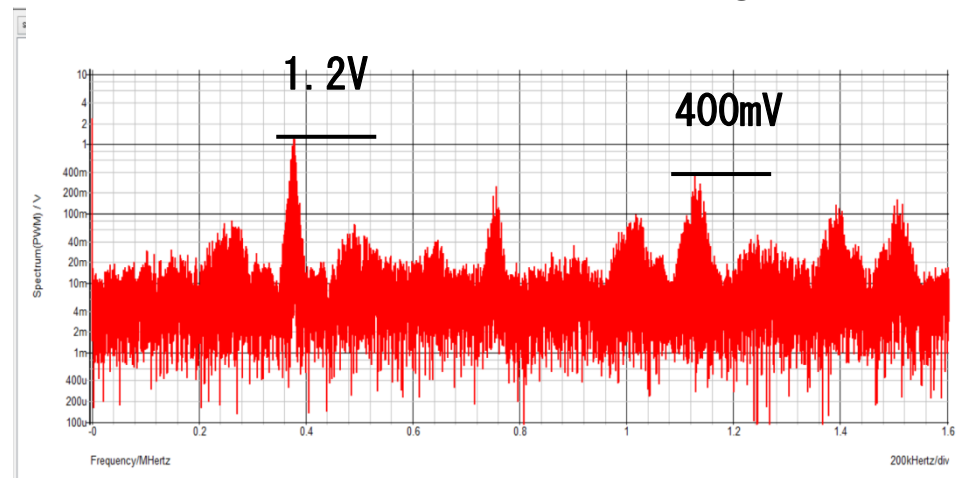


Fig.21 Ripple with Spread Spectrum



(a) Spectrum without Analog Noise



(b) Spectrum with Analog Noise

Fig.22 Spread Spectrum

# Conclusion

## 1. Buck Converter with ZVS-PWM Control

a) Simulation Result : Efficiency  $\eta$  (%)

\* SISO :  $\eta = \text{MAX } 95.5$  ( $\Delta \eta = 1.2\%$  @  $I_o = 1.0\text{A}$  )

$\text{MAX } \Delta \eta = 6.5\%$  @  $I_o = 0.2\text{ A}$

\* SIDO :  $\eta = \text{MAX } 86.0$  ( $\Delta \eta = 7.5\%$  @  $I_o = 0.3\text{A}$  ) =  $\text{MAX } \Delta \eta$

b) Simulation Result : SIDO Converter

Output Ripple :  $\Delta V_o \doteq 10\text{mVpp}$  @  $I_o = 0.5/1.0\text{ A}$

Over-shoot :  $\pm 10\text{mV}$  @  $\Delta I_o = \pm 0.5\text{ A}$

## 2. Proposed Spread Spectrum

a) New Spread Spectrum with Pseudo Analog Noise

3-bit M-sequence + LPF  $\Rightarrow$  Add to Voltage reference

b) Spectrum Reduction

\* Basic frequency :  $-4.0\text{dB} : 1.2\text{V} \leftarrow 3.0\text{V}$  ( $F = 377\text{ kHz}$ )

\* Harmonic freq. :  $-3.5\text{dB} : 0.4\text{V} \leftarrow 0.9\text{V}$  ( $F = 1.13\text{MHz}$ )

Thank you  
for your attention.